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HOT-GAS PRESSURE-FILTER APPARATUS

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CROSS-REFERENCE TO RELATED APPLICATIONS

5 This application claims the benefit of U.S. Provisional
Application No. 60/350,605, filed Jan. 22, 2002.

STATEMENT REGARDING FEDERALLY-SPONSORED RESEARCH
OR DEVELOPMENT

Not applicable

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REFERENCE TO MICROFICHE APPENDIX

Not applicable

BACKGROUND OF THE INVENTION

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This invention relates to a filter apparatus and method
of its operation, particularly to a pressure filter and method
for extracting liquids from wet slurry fluids and for
producing a substantially-dry filter cake of the solid
20 materials present in such slurry fluids.

In many industrial processes and other
applications where a slurry of solids and liquids is produced,
it becomes necessary to filter the slurry solids from the
liquids so that these materials may be efficiently utilized
25 or, alternatively, disposed in an environmentally-safe
manner. To separate the solids from the liquids, a filter
apparatus, such as a pressure filter, is often used. Known
pressure filters generally include one or more pairs of filter
plates capable of relative motion. The plate inlet is adapted
30 for receiving the slurry while the filtered liquids, called
the filtrate, are collected by means of the plate outlet which
also provides the requisite support for a filter medium
positioned between the filter plates. This arrangement
permits a filtration chamber to be defined by the inlet plate
35 and the filter medium when the plates are pressed together.
In the usual production cycle of such a filter, slurry is
introduced into the filtration chambers under pressure
through one or more inlet port, whereby it distributes itself
throughout the chamber. After the filtration chamber is

filled with slurry, the filter executes a series of programmed operations, namely, washing and/or treating the contents of the chamber in a particular manner, as well as pressurizing the chamber to force the liquids from the slurry through the filter medium, leaving the slurry solids, consolidated in a substantially-dry filter cake, within the chamber. The chamber is then opened, allowing the dry filter cake to be removed therefrom.

In the filter apparatus of the type here discussed, the filter is operated in a batch mode; i.e. apparatus open, apparatus closed, slurry input, treatment of the slurry to develop a cake, apparatus opened, filter medium moved as cake is discharged and advanced to the next cycle position, and then repeating the above steps. Efficiency of a pressure filter can be measured in the dryness of the resulting filter cake or in the success in removing a desired liquid from the slurry as effluent. The overall efficiency is measured in the amount of equipment and peripheral utilities that may be needed to accomplish a filter cycle as well as the length of time required for a single filter operation.

A need therefor arises for pressure-filter apparatus capable of efficiently treating a variety of slurries in a quick and low cost method. Furthermore it is desirable to provide a pressure-filter apparatus that is energy-efficient and capable of producing a substantially-dry filter cake in a minimum amount of time.

SUMMARY OF THE INVENTION

A pressure filter is disclosed. The filter apparatus includes two continuously mating surfaces movable relative to each other and a filter medium capable of being disposed therebetween. A surface is provided for supporting the filter medium. This supporting surface is bounded by and is, substantially coplanar with one of the continuous mating surfaces. The filter further includes an inlet cavity, bounded by the other of the continuous mating surfaces, and an inlet distributor in communication with the inlet cavity. When the mating surfaces are pressed together, a filtration chamber is defined by the inlet cavity and the filter medium.

The filter apparatus may include a plurality of filtration chambers, constructed as described above, a plurality of peripheral elements for introducing slurry, gasses and liquids to the filtration chamber, an exit port or ports for removing liquids and/or gasses from the chamber, the necessary valving systems, and control means for causing the sequential operation of the filter apparatus and its peripheral elements.

The advantages of the present invention will become apparent after consideration of the ensuing description and the accompanying drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

The present invention is illustrated by way of example and not by way of limitation, in the figures of the accompanying drawings, where:

FIG. 1 is a schematic sectional view of a pressure-filter apparatus and peripheral elements in accordance with one embodiment of the present invention.

FIG. 2 is a schematic sectional view of another embodiment of the invention.

FIG. 3 is a schematic sectional view of yet another embodiment of the invention.

FIG. 4 is a schematic sectional view of a filter apparatus including a vibrator attached to an element that forms a part of the filter chamber.

FIG. 5 is a perspective view of a means for cleaning the filter medium as used on one form of the invention.

FIG. 6 is a perspective view of an alternative form of an element of the cleaning apparatus of FIG. 5

FIG. 7 is an alternative form of filter medium cleaning apparatus.

FIG. 8 is a schematic diagram of the valving elements and their control in accord with one form of the present invention.

FIG. 9 is a chart showing possible operations and combination of operations of the chamber forming apparatus and the peripheral elements.

FIG. 10 is a steam vapor phase graph of temperature verses pressure.

For purposes of illustration, these figures are not necessarily drawn to scale. In all of the figures, like components wherever possible are designated by like reference numerals.

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DETAILED DESCRIPTION OF THE INVENTION

Throughout the following description, specific details are set forth in order to provide a more thorough understanding of the invention; however, the invention may be practiced without these particulars. In other instances, well known elements have not been shown or described to avoid unnecessarily obscuring the invention. Accordingly, the specification and drawings are to be regarded in an illustrative, rather than a restrictive, sense.

15 FIG. 1 is a schematic view of a pressure-filter apparatus according to one embodiment of the present invention. The apparatus includes an inlet plate 100 and an outlet plate 102, movable relative to each other, with a filter medium 104 capable of being disposed therebetween. Inlet plate 100 has
20 an inlet cavity 106 as well as an inlet port(s) 108 in communication with cavity 106 and inlet piping (header) 109. Inlet port 108 may be horizontal, as shown in FIG. 1, or may be vertically disposed. Furthermore, separate inlet ports for gasses and liquids may be utilized. Inlet cavity 106 is
25 bounded by a continuous mating surface 110. Outlet plate 102 incorporates a grid 112, which provides a supporting surface for filter medium 104. This supporting surface is bounded by and substantially coplanar with (e.g., within approximately 1/16 of an inch (1.0mm)) a continuous mating surface 114.
30 Plate 102 further includes an outlet cavity 116 for collecting the filtrate liquids and an exit port 118 for discharging the filtrate, which may then undergo further processing or be properly disposed. Exit port 118 leads into a filtrate line 122. As viewed from the top, the peripheral shape of plates
35 100 and 102 may take any form, but is usually rectangular or circular.

When plates 100 and 102 are pressed together, as illustrated in FIG. 1, a filtration chamber 120 is defined by inlet cavity 106 and filter medium 104. It should be

understood that the longitudinal and transverse dimension of the filter medium inside chamber 120 exceed the corresponding dimensions of inlet cavity 106. The depth of the filtration chamber may vary from about 0.25 of an inch (one centimeter) to about 8 inches (20 centimeters), depending on the particular application. An inlet distributor may be disposed between inlet port 108 and cavity 106 to promote an optimal dispersion of slurry within the filtration chamber and to allow subsequent application of pressurized fluids without disturbing the uniform distribution of slurry inside the filtration chamber.

FIG. 1 provides only a schematic representation of the filter-plate configuration and certain elements of the apparatus either have not been shown or have been shown in simplified form to avoid unnecessarily obscuring the invention, for example, continuous mating surfaces 110 and 114 may contain recessed grooves having fluid connections P1 and P2 for providing an effective seal between the mating surfaces of the filter plates to substantially reduce or completely eliminate leakage of slurry fluids between the filter plates. The specific details of such an arrangement is disclosed in U.S. Patent No. 5,059,318, which is hereby incorporated by reference. Similarly, grid 112 represents only one possible structure for providing the requisite supporting surface for the filter medium 104. Other alternatives for supporting the filter medium, as well as specific arrangements and construction of the filter plates, the filter medium, and other components of the filter apparatus have been disclosed in U.S. Patents No. 5,292,434, 5,462,677, 5,510,025, 5,573,667, 5,615,713, and 6,491,817, all of which are hereby incorporated by reference. Even though inlet cavity 106 has been schematically illustrated in FIG. 1 as having square corners and vertical side walls, in practice it may be beneficial to provide an inlet cavity incorporating tapered side walls and radiused corners (not shown) to prevent the filter cake from adhering to the inside of inlet plate 100.

Referring once again to FIG. 1, in one embodiment of the invention the pressure-filter apparatus includes a slurry source 124 coupled with inlet piping 109 via a shut-off valve

B. A source 126 of hot gas is coupled with inlet piping 109 through a shut-off valve A. Header 109 includes a drain valve C.

5 Source 126 comprises a holding tank whose pressure is maintained by, e.g., at least one compressor, boiler, or gas generator. Source 124 comprises a slurry-holding tank having at least one pressure-supply apparatus, such as a conventional pump.

10 Depending on the specific application, different combinations of fluids and pressures in tanks are possible. For example, the slurry supplied from sources 124 may be maintained at a pressure up to about 300 psi. Similarly, source 126 may contain hot gasses pressurized up to about 500 psi. Source 126 may contain a variety of hot gasses, e.g.,
15 steam maintained at a temperature from about 200°F to about 500°F or air/inert gasses maintained at a temperature up to about 550°F.

FIG. 1 OPERATION SEQUENCE, OPEN LOOP

- 20 1. Plates are closed. Valves A, B, and C are closed.
2. Valve B is opened to fill the filtration chamber with slurry. Valve B is closed once the filtration chamber is filled and the cake is formed therein. The duration of opening for valve B can be determined based on elapsed time or
25 by measuring back-pressure inside the filtration chamber with a pressure sensor (e.g., valve B is closed when the back pressure inside the filtration chamber approaches the slurry-input pressure). Alternatively, valve B may be shut off when a flow meter indicates that the flow rate of slurry has
30 decreased to a predetermined value or that a predetermined quantity of slurry has entered the chamber. In yet another embodiment of the invention, valve B maybe shut off when a load cell determines that the contents of the filtration chamber have reached a specific weight. As an optional step, header-drain valve C may be opened to drain the slurry from the header;
35 valve C is then closed.
3. Valve A is opened and hot pressurized gas (e.g., steam, air or inert gas such as nitrogen) is introduced into the filtration chamber to force the liquids from the slurry cake.

The shut-off point of valve A may be determined, e.g., by a pressure sensor located inside the filtration chamber or in the inlet piping. Alternatively, the shut-off point of valve A may be based on elapsed time, weight loss, or rate of fluid out of the filtration chamber.

4. Header drain valve C is opened to vent any residual pressure in the filtration chamber above the cake. Next, the plates are opened so the cake can be removed from the filtration chamber by advancing the belt.

FIG. 2 illustrates another embodiment of the invention, where the pressure-filter apparatus includes a slurry source 124, a source 126 containing hot gas, a source 128 containing wash fluid, a source 130 containing gas at conventional pressure, and a source 132 containing gas at elevated pressure. Sources 124, 126, 128, 130 and 132 are coupled with header 109 via shut-off valves B, A, D, E and F respectively.

Depending on the specific application, different combinations of fluids and pressures in the tanks comprising sources 124-132 are possible. For example, the slurry supplied from source 124 may be maintained at a slurry-input pressure up to about 300 psi. Similarly, source 126 may contain a hot gas at a pressure up to 500 psi. Source 126 may contain a variety of hot gasses, e.g., steam maintained at a temperature up to about 550°F. Wash fluid, which may be a liquid or a gas, in source 128 may be at an elevated temperature and may be maintained at a pressure up to about 300 psi. Sources 130 and 132 may be maintained at a temperature up to about 550°F and may be maintained at pressures up to about 150 psi (conventional pressure) and up to about 500 psi (elevated pressure), respectively, and may contain gasses such as air or inert gas such as nitrogen. In this particular embodiment of the invention, for any given application, source 132 will be maintained at a higher pressure than that of source 130, i.e., elevated pressure is always higher than conventional pressure. In some cases, pressure in sources 128 will be higher than that in sources 124.

FIG. 2 OPERATION SEQUENCE, OPEN LOOP

1. Plates are closed. Valves A, B, C, D, E and F are closed.

2. Valve B is opened to fill the filtration chamber with slurry. Valve B is closed once the filtration chamber is filled and a cake is formed therein. The duration of opening of valve B can be determined in substantially the same manner as described above with respect to the apparatus of FIG. 1. As
5 the slurry from the header; valve C is then closed.

3. Optionally, valve D is opened to introduce the cake-wash fluid into the filtration chamber. Once the washing
10 operation is completed, valve D is closed. The duration of this step may be based, e.g., on elapsed time or on decreased weight of the contents of the chamber. Alternatively, valve D may be closed when a flow meter indicates that the flow rate of
15 wash fluid has reached a predetermined value or that a predetermined quantity of wash fluid has entered the filtration chamber or the desired properties in the effluent have been reached. Header drain valve C may also be opened to drain the cake-wash fluid from the header, valve C is then closed.

20 4. Valve F is opened and gas at elevated pressure or elevated pressure and temperature is introduced into the filtration chamber to force the liquids from the slurry cake. The shut-off point of valve F may be determined, e.g., by a pressure sensor located inside the filtration chamber or in the inlet
25 piping. Alternatively, the shut-off point of valve F may be based on elapsed time, decrease in weight of the contents of the filtration chamber, or flow rate of fluid out of the chamber.

30 5. When the residual pressure in the filtration chamber drops sufficiently to be substantially equal to conventional pressure, valve E is opened and gas at conventional pressure or conventional pressure with elevated temperature is introduced into the filtration chamber to force the residual liquids from the slurry cake. The shut-off point of valve E may be
35 determined in substantially the same manner as that of valve F in the preceding step.

6. Valve A is opened and hot gas (e.g., steam, air or inert gas such as nitrogen) is introduced into the filtration chamber to force any residual liquids from the slurry cake and

to dry the cake. The shut-off point of valve A may be determined, e.g., based on back-pressure inside the filtration chamber, elapsed time, or a combination of these parameters.

5 7. Header drain valve C is opened to vent any residual pressure in the filtration chamber above the cake. Next, the plates are opened so that the cake can be removed from the filtration chamber by advancing the belt.

FIG. 3 illustrates yet another embodiment of the
10 invention, where the pressure filter apparatus includes a slurry source 124, a source 126 containing hot gas, a source 128 containing wash fluid, and a source 134 also containing hot gas. Hot gas source 134 is coupled with a conventional automatic system pressure and heat recovery unit 136.
15 Sources 124, 126, 128 and 134 are coupled with header 109 via shut-off valves B, A, D and G, respectively. Filtrate line 122 discharges into a filtrate tank 138 through a shut-off valve I. Filtrate line 122 further includes a filtrate vent 140, terminating in a shut-off valve H. Filtrate tank 138 is
20 coupled with hot-gas source 134 and is at the same pressure therewith.

Depending on the specific application, different combinations of fluids and pressures in the tanks comprising sources 124, 128, 126 and 134 are possible. For example, the
25 slurry supplied from source 124 may be maintained at a pressure up to about 300 psi. Source 126 may contain a hot gas at a pressure up to about 500 psi. Source 126 may contain a variety of hot gasses, e.g., steam maintained at a temperature of about 200°F to about 550°F or air/inert gasses maintained at a
30 temperature up to about 550°F. Similarly, source 134 may contain a hot gas at a pressure up to about 150 psi (system pressure). Source 134 may contain a variety of hot gasses, e.g., steam maintained at a temperature from about 200°F to about 360°F or air/inert gasses maintained at a temperature up
35 to about 550°F. Wash fluid in source 128 may be maintained at a pressure up to about 300 psi and/or at temperature 550°F. In this particular embodiment of the invention, for any given application, system pressure is lower than the pressures maintained in sources 124, 126 and 128. In some cases,

pressure in source 128 will be higher than that in source 124.

FIG. 3, OPERATION SEQUENCE, CLOSED LOOP

1. Plates are closed. Valves A, B, C, D, G, H and I are closed.
2. System is pressurized by opening valve G. As an optional step, while valve G is open, valve H may be opened to preheat the filtration chamber and to purge preexisting air from the chamber. Valve H is then closed, followed by closing valve G. After valve H is closed, valve G should remain open long enough so that the pressure in the filtration chamber becomes equal to system pressure.
3. Valve I is opened.
4. Valve B is opened to fill the filtration chamber with slurry. Valve B is closed after the slurry fill is complete. The duration of opening of valve B can be determined in substantially the same manner as described above with respect to the apparatus of FIG. 1. As an optional step, header drain valve C may be opened to drain the slurry from the header; valve C is then closed.
5. Optionally, valve D is opened to introduce the cake-wash fluid into the filtration chamber. Once the washing operation is completed, valve D is closed. The duration of this step may be based, e.g., on elapsed time. Alternatively, valve D may be closed when a flow meter indicates that the flow rate of wash fluid is decreased to a predetermined value or that a predetermined quantity of wash fluid has entered the filtration chamber. Header drain valve C may also be opened to drain the cake-wash fluid from the header; valve C is then closed.
6. Valve A is opened and hot gas is introduced into the filtration chamber to force the liquids from the slurry cake. The shut-off point of valve A may be determined based on the back pressure inside the chamber, elapsed time, decrease in weight of the contents of the chamber, or a combination of these parameters. As an option, while valve A is open, flow of hot gas through valve I may be restricted to maximize the interaction dwell time between the hot gas and the filter cake.
7. Valve I is closed to prevent system pressure from

entering lower plate 102.

8. Valve H is opened to vent pressure below the cake.

9. Valve C is opened to vent any residual pressure in the filtration chamber above the cake. Next, the plates are opened so the cake can be removed from the filtration chamber by advancing the belt.

In yet another embodiment of the invention, the pressure-filter apparatus includes a vibrator 200, attached to inlet plate 100, as shown in FIG. 4. The vibrator serves to help dislodge residual fragments of the cake continuing to adhere to the inlet plate after the dry cake has been removed from the filtration chamber at the end of the filtration cycle. In one embodiment of the invention, the vibrator may be pneumatically or electrically operated. Proximity switches 202 and 204 are positioned such that vertical motion of plate 100 causes the switches to be activated. The switches are coupled to a programmable logic controller 80 shown schematically in FIG. 8.

FIG. 4, OPERATION SEQUENCE, VIBRATOR

1. As the plates begin to open (i.e., plate 100 is raised), the vibrator is turned on by the programmable logic controller.

2. The plates stop opening when the proximity switch 204 is activated by upward motion of plate 100.

3. Belt 104 is moved from the filtration chamber and discharges the cake.

4. Plates begin to close (i.e., plate 100 is lowered). As switch 202 is activated, the downward motion of plate 100 is arrested. The vibrator is then turned off and the drive of belt 104 is activated once more to discharge any remnants of the cake dislodged by the vibrator and is then stopped in the "home" position.

5. Plates close.

Those skilled in the art will appreciate that depending on the application, various modes of operation of the vibrator are possible, including continuous operation without shutdown.

In yet another embodiment of the invention, depicted with reference to FIG. 5, the pressure-filter apparatus may include

a brush 300 provided for cleaning belt 104. The brush has patterned bristles 301 and is coupled by a conventional drive mechanism 302, e.g., a chain drive, to a belt pulley 115, which may be driven by a motor 117. Two examples of a plurality of possible bristle patterns are illustrated in FIGs. 5 and 6. Bristle 301 may have variable stiffness, from coarse to soft. Drive mechanism 302 may incorporate a brush-adjustment mechanism. In one embodiment, the gearing of drive mechanism 302 and the diameters of the brush and the belt pulley may be selected such that the linear speed of the brush is four times that of the linear speed of the belt. Other ratios between belt speed and brush speed may be beneficial, depending on the application. Brush 300 may also be powered by a dedicated motor or may be geared to an idler pulley at the opposite end of the filter. Brushes at both ends of the filter may also be utilized. A collection bin 304 is used to gather the debris dislodged by the brush(s).

As shown in FIG. 7, in yet another embodiment of the invention, the pressure-filter apparatus may include a roller 400 with substantially-rigid vanes or cup wipers 402 for cleaning the belt. Roller 400 may be driven in a manner substantially similar to that of brush 300 described with reference to FIG. 5. Roller 400 may also be used in combination with brush 300.

FIG. 8 is a schematic diagram of an embodiment with one possible set of valving elements and their control in operating a filter apparatus in accord with the present invention. A filter chamber 120 is produced by the inlet plate 100 and the outlet plate 102 with the filter medium 104 disposed therebetween. As illustrated there are sources of several fluids and gasses with output controlled by valves and a programmable controller 80 through input and output connection illustrated by dotted lines from the controller to the valves and reverse. The controller 80 also includes elements for programmed control of the closing and opening of the inlet plate 100 and outlet plate 102. The controller may be supplied with the pressure, temperature and level sensors within the filter chamber for the purposes that have previously been described.

As illustrated, an inlet for slurry feed 801 is connected through valve B to an input header 800. The header 800 is represented by a single line; however, it should be understood that the single line represents the input of slurry and various gasses and a liquid into plate 100. A discharge header 808 is shown for effluent filtrate liquids and/or gasses from plate 102 for the filter apparatus as illustrated in FIG. 1.

Connected to the input header 800 at the discharge end is an outlet for header drain 102 through valve C for draining slurry feed after the chamber has been filled. Connected to the input header 800 at the input end is an inlet for blowdown gas 803 through valve E/F, an inlet for wash fluid 806 through valve D, an inlet for steam 809 through valve A. Each of the valves E/F, D and A being controlled by and having feedback to the controller 80.

A seal air source 805 is connected through a valve P1/P2 for the purpose described with respect to FIG. 1. An inlet for belt wash source 804 controlled through valve W is operated by the controller 80.

Dotted lines from the chamber 120 and from the belt drive system illustrate control from and feedback to the controller 80 for opening and closing the chamber and for operating the inlet of belt wash 804 (or the brush system of FIGs. 5-7) to clean the filter medium 104 when the inlet plates 100 and 102 are separated in preparation for reentry into the apparatus when the next filter cycle is initiated.

Discharge header 808 is connected to a main outlet 811 through a suitable valve 812 and to a restricted outlet 813 through a valve 814 and an adjustable valve 815. The discharge header 808 carries effluent filtrate and any wash fluids or gasses that pass through the filter cake formed within the chamber 120. Those fluids may be used to pretreat input fluids or may be connected to collection apparatus. When the chamber 120 is to be pressurized (before, during or after slurry input), the valve 815 is used to maintain a desired system pressure. All of these valves can be under control by the controller 80.

Because the filter apparatus operated in accord with the present invention can produce differing filtrates based on the

input of air, hot air, hot gases, steam or wash fluids of different chemical composition, there can be different filtrates produced at different times during the operation. In some cases the filtrate can be the desired product and/or the filtrate can be recirculated to pretreat certain of the input materials to the apparatus. FIG. 8 also illustrates an outlet for slurry recirculation 810 operated by valve I under control of the controller 80. The recirculated filtrate is available for recirculation to pretreat, for example, the slurry input 801, the inlet blow down gas 803, the inlet of wash fluids 806 or the inlet for steam 809.

FIG. 9 is a representative example of possible sequence of operation of the valves of FIG. 8 under control by the controller 80. In the chart of FIG. 9 "C" represents a closed valve, "O" an open valve and an asterisk "*" by an "O*" or "C*" indicates optional operation of the respective valve during an operation of the apparatus. The chart represents a complete cycle of a filter apparatus in accord with the present invention from plate closing, slurry filling, cake wash, blowdown, open plates and cake discharge.

The operation of the filter apparatus in accord with the present invention permits the treatment of slurry to separate the slurry into slurry solids and slurry liquid. The present apparatus can be operated at pressure below atmospheric (vacuum) or at elevated pressure up to about 500 psi. The apparatus can operate with temperatures in the range of ambient to about 550° F so as to treat slurries at varying temperature ranges. Under the control of a suitable controller, the apparatus can be programmed to treat slurries in a sequence of hot air, hot gasses, liquids and/or steam in repeated sequences. In some cases the chamber is filled with slurry, then dewatered, then filled again in one or more cycles. A particular advantage is available because the filter chamber can sustain elevated pressure and, under such pressures, steam passing through the filter cake formed in the chamber can remain dry while transferring useful heat to the filter cake.

FIG 10 illustrates a well known vapor phase diagram of steam illustrating in the "x" axis temperature and in the "y"

axis pressure. The plotted line represents the transition of vapor to dry steam at a temperature and pressure.

The use of dry steam is a particularly desirable feature for the treatment of those slurries where the resultant filter cake is improved when heated but cannot withstand wet treatment while heated. A variety of temperature and pressure treatments can be treated with the present apparatus.

The use of hot gas as a slurry treatment has been shown to improve the efficiency of the separation process and has permitted the production of a drier filter cake in discharge from the apparatus. Combinations of hot gas, inert gasses and steam have produced improved quality filter cake and/or filtrate and have been shown to reduce the amount of utilities needed to produce a dry filter cake.

As a side requirement in the treatment of slurries that produce a filter cake that cannot be subject to moist conditions, the present invention provides for the dry treatment in cleaning a filter medium. Residual liquid on a belt cleaned with wash fluids can cause adverse conditions within the filter chamber. With the dry filter belt cleaning system of FIGs. 5-7, the filter medium 104 is brushed by brush 300 having a pattern of bristles 103 that effectively removes residual filter cake solids from the medium 104. The brush cleaning can be effected at both ends of the apparatus; i.e., when the belt leaves the chamber and again before it reenters the chamber.

The belt illustrated in the FIGs. 5-7 and described above for cleaning is a filter medium that collects the solids of the slurry when the liquids are forced out as effluent. The filter medium may be specifically designed for the particular slurry being separated and particularly for the pressure and temperature ranges to be encountered within the filter chamber in a slurry separation process. Filter medium of various constructions are described in U.S. Patent 5,462,677, 5,477,891 and 5,615,713 which are incorporated by reference.

Some of the features of the present apparatus and its operation permit the reduction in utilities needed for completing a filter operation. One such reduction is accomplished by using hot air in forcing fluids from the slurry

within the chamber. The usual compressor that supplies high pressure air heats the air in the process of increasing its pressure. Frequently, such air compressors are equipped with an air cooler in a system that passes the compressed air to an accumulator. With the present apparatus, that cooler can be eliminated because the filter apparatus can accommodate the high pressure air and high pressure air at elevated temperature. If the slurry being filtered to produce a desired filter cake can accept the elevated temperature filter gas, the cost of operating a compressed gas cooler can be eliminated, thus reducing that utility cost.

Another utility cost saving can be available through the discharge of hot filter cake from the filter apparatus. Some filter systems discharge a filter cake that must be further dried by being passed into a dryer. With the present invention, a substantially dry filter cake can be created and discharged at an elevated temperature. Such a filter cake discharge can completely eliminate the need for additional drying and thus eliminate another utility expense.

Some filtration processes require a cooled filter cake while the creation of the cake can be produced in a more efficient manner if hot gas or steam is used in the filtration process. In such a case, the present apparatus and its programmable controller can be programmed to cool the filter cake with cool dry air or gas within the chamber prior to the discharge of the cake from the chamber.

The processes of the present invention can be applied to the filter apparatus illustrated or may be applied to an expression filter that uses a diaphragm or flexible plate component to squeeze the slurry and cake formed to remove slurry liquids and/or, if cake wash is used, to squeeze and remove cake wash fluid(s). By proper design of such filters and filtration method, the slurry and/or cake can be treated with hot gas, hot inert gas, or steam prior to the squeeze of the diaphragm or flexible plate component, as well as after the cake is formed and/or squeezed; or combination treated with hot gas, hot inert gas, or steam both prior to squeezing and after squeezing. In the case of dual-sided filtration or dual-sided filtration expression filters with filter medium

on both sides of the cake forming area, the hot gas, hot inert gas, and/or steam can be applied through the filter medium into the cake, or between the filter medium where cake is formed.

Often, a more efficient filtration process is accomplished with the present filter apparatus. However, it should be noted that the methods of the present invention can be applied to other filters.

An understanding of the difference between wet steam and dry steam is helpful in appreciating the advantages of the present hot gas and steam drive for removing liquids from a slurry. The vapor phase of steam is determined by the temperature and the pressure of the steam. Considering a Pressure/Temperature graph as illustrated in FIG. 10 of the drawings it can be seen that if the temperature of the steam is maintained above a temperature to the right of the vapor phase curve, the steam will always be "dry" and not precipitate water onto a filter cake. In the same way, if the pressure of the steam is maintained above the left of the curve, the steam will be "dry" at that temperature. This condition is of particular advantage to the present apparatus because the chamber of the filter apparatus can be closed and the pressure within the chamber can be elevated to as high as 500 psi. Likewise, the chamber can be evacuated to create a vacuum within the chamber to reduce the temperature of the steam within the chamber when "dry" steam is desired. The chamber can be operated at -8.0 psi. A reference to standard steam tables well known in the art will show that the boiling point of water can be reduced in a vacuum or increased in a pressurized system. Steam for the present invention can be used in the temperature ranges of about 80°C to about 230°C. If the slurry being filtered cannot withstand high temperature, a vacuum can be created within the chamber. If the slurry can withstand elevated temperature, the chamber can be pressurized and steam can be passed through the cake in the filtration process. In both cases, the pressure and temperature within the chamber can be controlled to keep the desired "dry" quality of the steam. Steam is a more efficient heat transfer material because it can be maintained "dry" by controlling the pressure of the steam.

With the present invention and the control of the passage

of filtrate and filter cake, the heat created during the filtration process can be recovered by pretreating the slurry or hot gasses with the heated products of the filtration process. The hot or heated filtrate can be recirculated into contact with the slurry or used to preheat the chamber or filtration gasses.

The filter apparatus can be controlled by a programmable controller in many differing cycles; those cycles being determined by the desired quality of the filtrate or the filter cake. In some cycles, a wash fluid is first passed through the filter cake to extract certain materials or liquids from the slurry. Those materials or liquids can be withdrawn from the filter chamber to a selected discharge location. The later extraction of liquids from the cake can be a different effluent and may be sent to a different location. The controller controls the operation of several separate valves that introduce different materials to the filtration chamber. Those materials can be used to preheat the chamber, to introduce the slurry, to introduce wash fluids, to introduce hot gas, inert gas or steam, in any desired sequence or repeated sequence. The objective of the filtration process may be to produce a desired filter cake or a desired effluent and the apparatus can be operated to produce the desired end products.

While certain preferred embodiments of the invention have been specifically disclosed, it should be understood that the invention is not limited thereto as many variations will be readily apparent to those skilled in the art and the invention is to be given its broadest possible interpretation within the terms of the following claims.